



Continuum Damage Mechanics Model and Calving Law

Elmer/Ice Users Meeting

Tuesday, April 9th, 2013

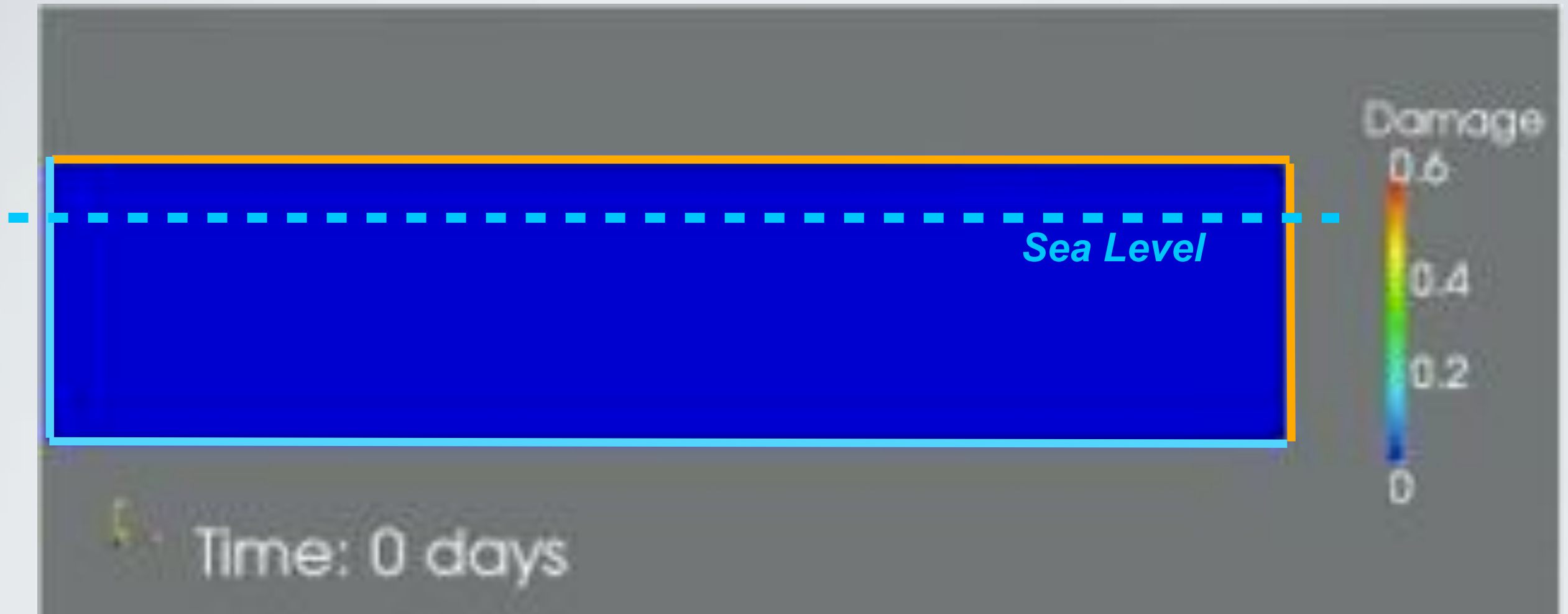
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Université Joseph Fourier*

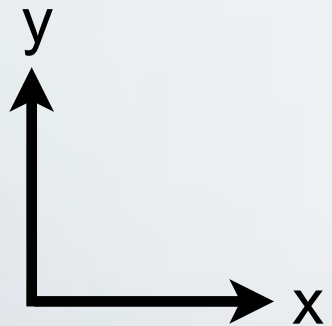


Contact : jean.krug@ujf-grenoble.fr

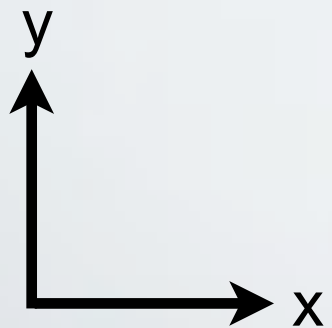
Imagine a marine-terminated grounded glacier...



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Imagine a marine-terminated grounded glacier...



Outline

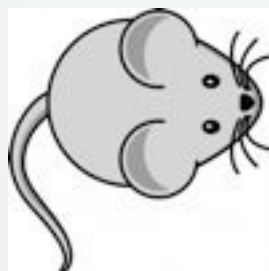
1/ Damage Model

2/ Calving Criterion

3/ Conclusion

4/ Special Bonus

Software Elmer/Ice, finite element model.
Full-Stokes model.



Model Presentation

Continuous Damage Mechanics Model

Damage Mechanics

1/ Subcritical crack propagation (Weiss, 2004)

Calving Solver

Linear Elastic Fracture Mechanics

2/ Fracture initiation (Van der Veen, 1998ab)

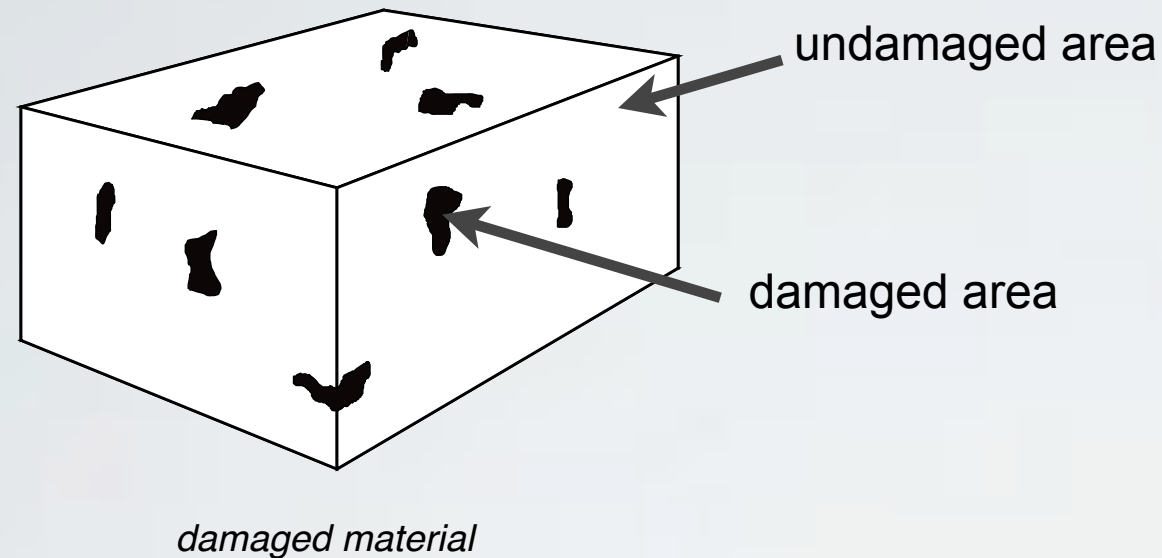
3/ Fracture arrest

Model Presentation - Continuum Damage Mechanics

Continuum Damage Mechanics (CDM) model : Local evolution of crevassing at the model grid scale, depending on the stress field and its transportation through a damage variable, which affects in turn the rheology of the ice.

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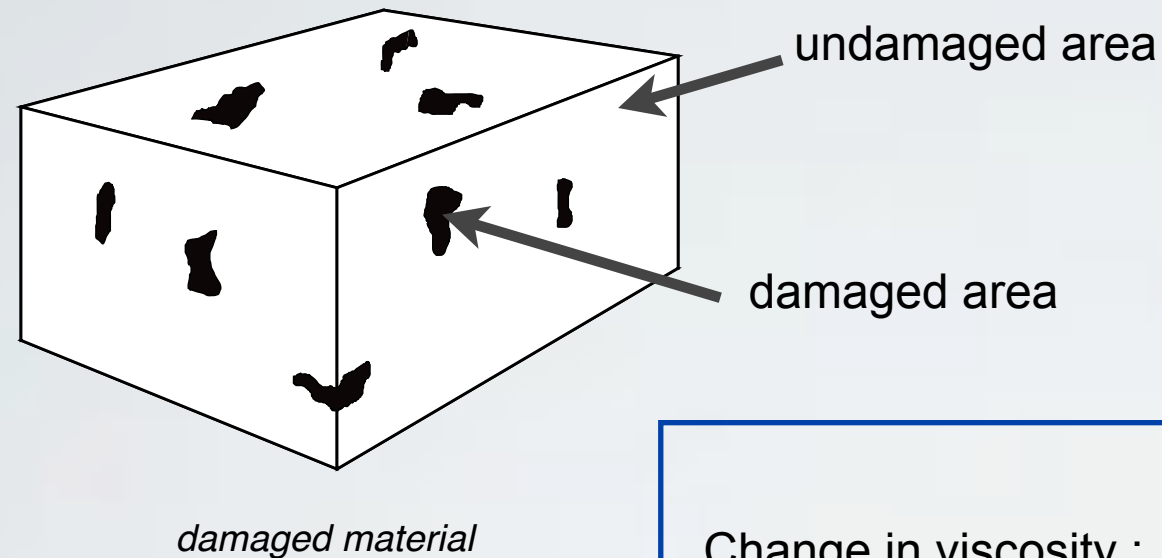


Isotropic damage variable \mathbf{D} :

$$\begin{cases} D = 0 & \text{Undamaged ice} \\ D = 1 & \text{Fully damaged ice} \end{cases}$$

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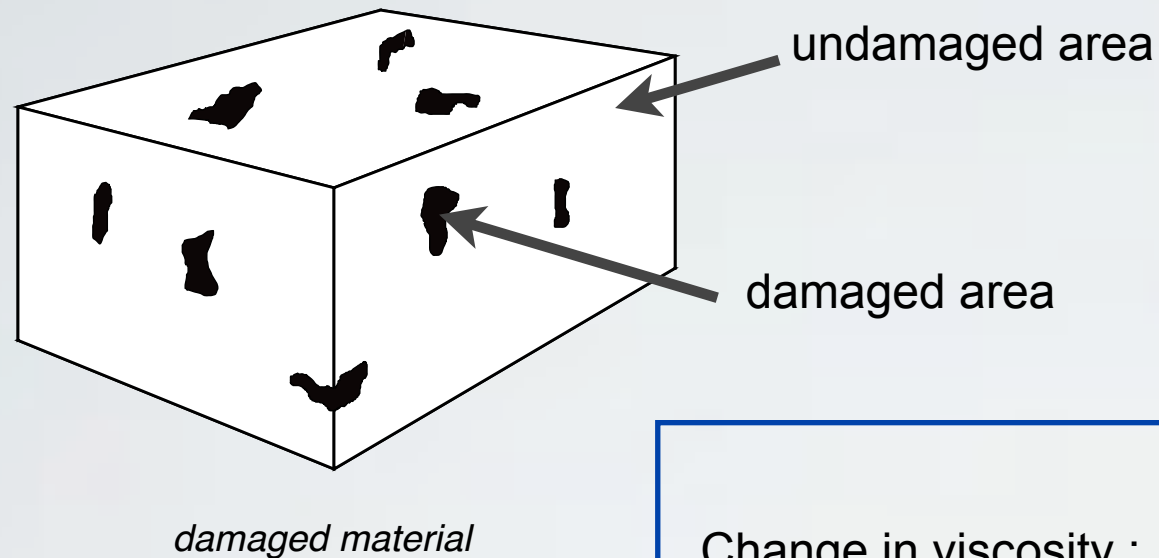
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Change in viscosity :

$$\mu = E \cdot f(\sigma) \quad \text{with} \quad E = \frac{1}{(1 - D)^n}$$

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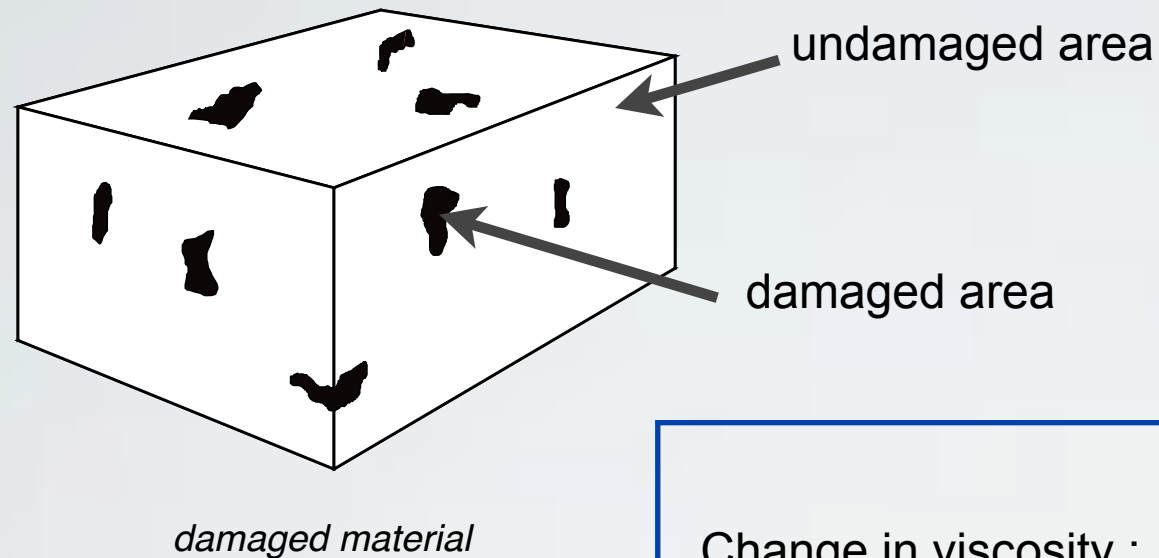
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Damage Variable is advected :

$$\frac{\partial D}{\partial t} + \vec{u} \nabla D = f(\chi)$$

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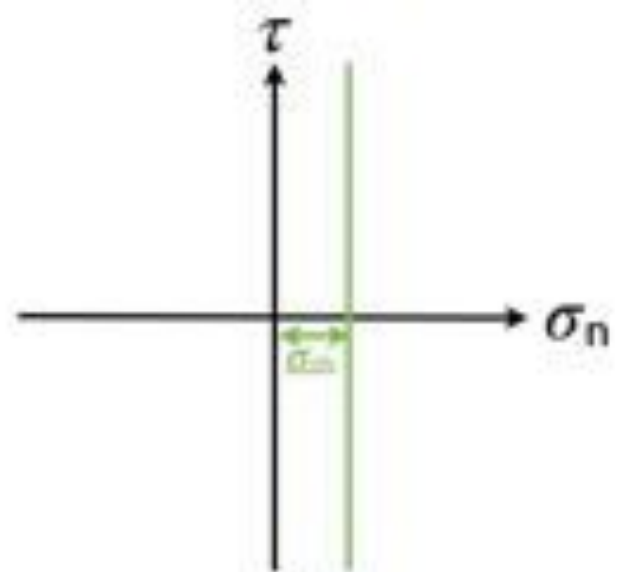
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Damage Variable is advected :

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Stress criterion for damage increase :

$$\chi(\tilde{\sigma}) = \frac{\sigma_I}{(1 - D)} - \sigma_{th}$$



Limit of the damage criterion. Stresses are positive in traction

Model Presentation - Continuum Damage Mechanics

Damage Mechanics

1/ Subcritical crack propagation (Weiss, 2004)

2/ Fracture initiation (Van der Veen, 1998ab)

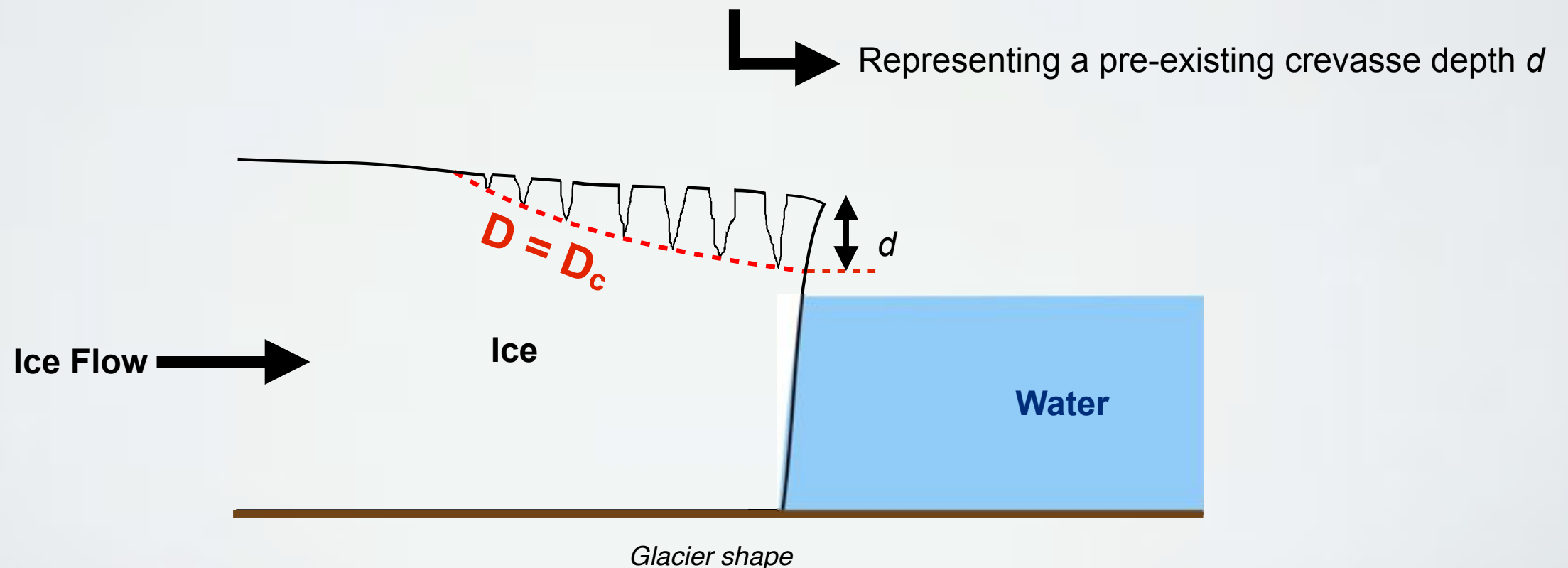
3/ Fracture arrest

Damage is free to evolve, slowly.

Ice keeps a viscous behaviour.

The viscosity and the ice flow are affected

Looking for a critical damage contour $D = D_c$.



Model Presentation - Continuum Damage Mechanics

USF_Damage.f90

InitDamage

Put some damage in the ice following a gaussian distribution

EnhancementFactor

Change the value of Glen Enhancement Factor

$$E = \frac{1}{(1 - D)^n}$$

```
Initial Condition 1
Pressure = Real 0.0
Velocity 1 = Real 0.0
Velocity 2 = Real 0.0
DID = Variable Damage
Real Procedure "/USF_Damage" "InitDamage"
End
```

+

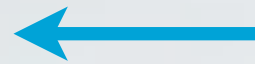
Boundary Conditions

```
Material 1
Density = Real 900

Viscosity Model = String "Glen"
Glen Enhancement Factor = Variable Damage
Real Procedure "/USF_Damage" "EnhancementFactor"
```

Model Presentation - Continuum Damage Mechanics

InitDamage



USF_Damage.f90



EnhancementFactor



SourceDamage

Compute the source term of the advection equation

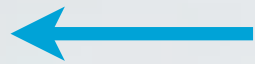
Compute Principal
stresses



ComputeDevStress

Model Presentation - Continuum Damage Mechanics

InitDamage



USF_Damage.f90



EnhancementFactor



SourceDamage

Compute the source term of the advection equation

Compute Principal stresses



Compute the damage criterion

$$\chi(\tilde{\sigma}) = \frac{\sigma_I}{(1 - D)} - \sigma_{th}$$



ComputeDevStress

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Compute the source term of the advection equation

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Compute the damage criterion

$$\chi(\tilde{\sigma}) = \frac{\sigma_I}{(1 - D)} - \sigma_{th}$$

Compute the source term

$$f(\chi) = B \cdot \chi$$

ComputeDevStress

```
Body Force 1
Flow BodyForce 1 = Real 0.0
Flow BodyForce 2 = Real $gravity
DGD Source = Variable Damage
Real Procedure "./USF_Damage" "SourceDamage"
End
```

$$\frac{\partial D}{\partial t} + \vec{u} \nabla D = f(\chi)$$

Model Presentation - Continuum Damage Mechanics

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USF_Damage.f90

EnhancementFactor

SourceDamage

Compute the source term of the advection equation

Compute Principal stresses

Compute the damage criterion

$$\chi(\tilde{\sigma}) = \frac{\sigma_I}{(1 - D)} - \sigma_{th}$$

Compute the source term

$$f(\chi) = B \cdot \chi$$

ComputeDevStress

Criterion name

B

σ_{th}

Healing factor

```
! Damage Source Parameters
Damage Criterion = string "Krug"
Damage Enhancement Factor = Real 20.0
Damage Parameter sigmath = Real 0.04
Damage Parameter lambdah = Real 0.4
```

```
Body Force 1
Flow BodyForce 1 = Real 0.0
Flow BodyForce 2 = Real $gravity
DGD Source = Variable Damage
Real Procedure "./USF_Damage" "SourceDamage"
End
```

$$\frac{\partial D}{\partial t} + \vec{u} \nabla D = f(\chi)$$

Model Presentation - Linear Elastic Fracture Mechanics

LEFM

- 1/ Subcritical crack propagation (Weiss, 2004)
- 2/ Fracture initiation (Van der Veen, 1998ab)
- 3/ Fracture arrest

The stress intensity factor K_I is used to describe stress concentration near the tip of the crack.

$$K_I = \langle S_{xx} \rangle \sqrt{\pi d}$$

opening tensile stress minus closing
compressive cryostatic pressure

crevasse depth

The fracture propagates if $K_I > K_{Ic}$ (ice toughness)

Model Presentation - Linear Elastic Fracture Mechanics

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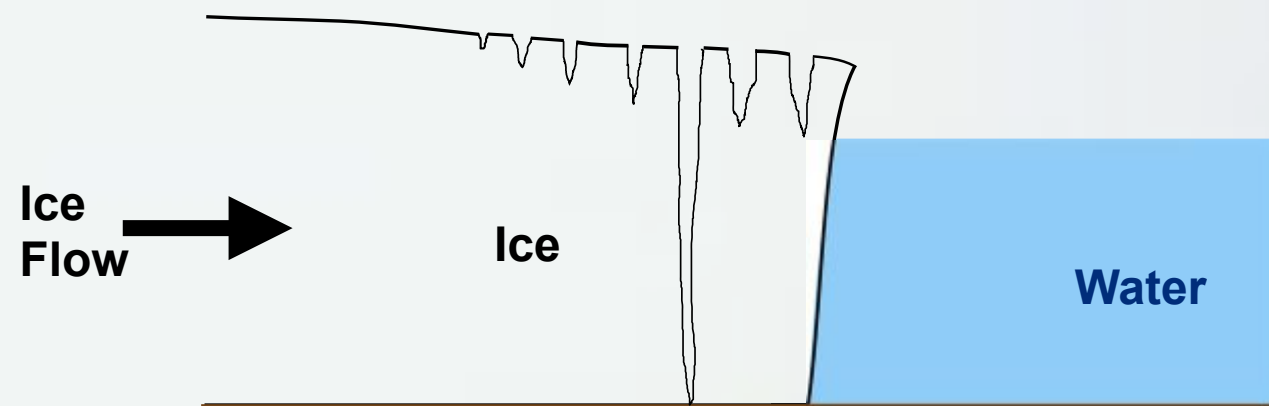
crevasse depth

The fracture propagates if $K_I > K_{Ic}$ (ice toughness)

K_{Ia} = arrest criterion

$$K_{Ia} = \alpha \cdot K_{Ic}$$

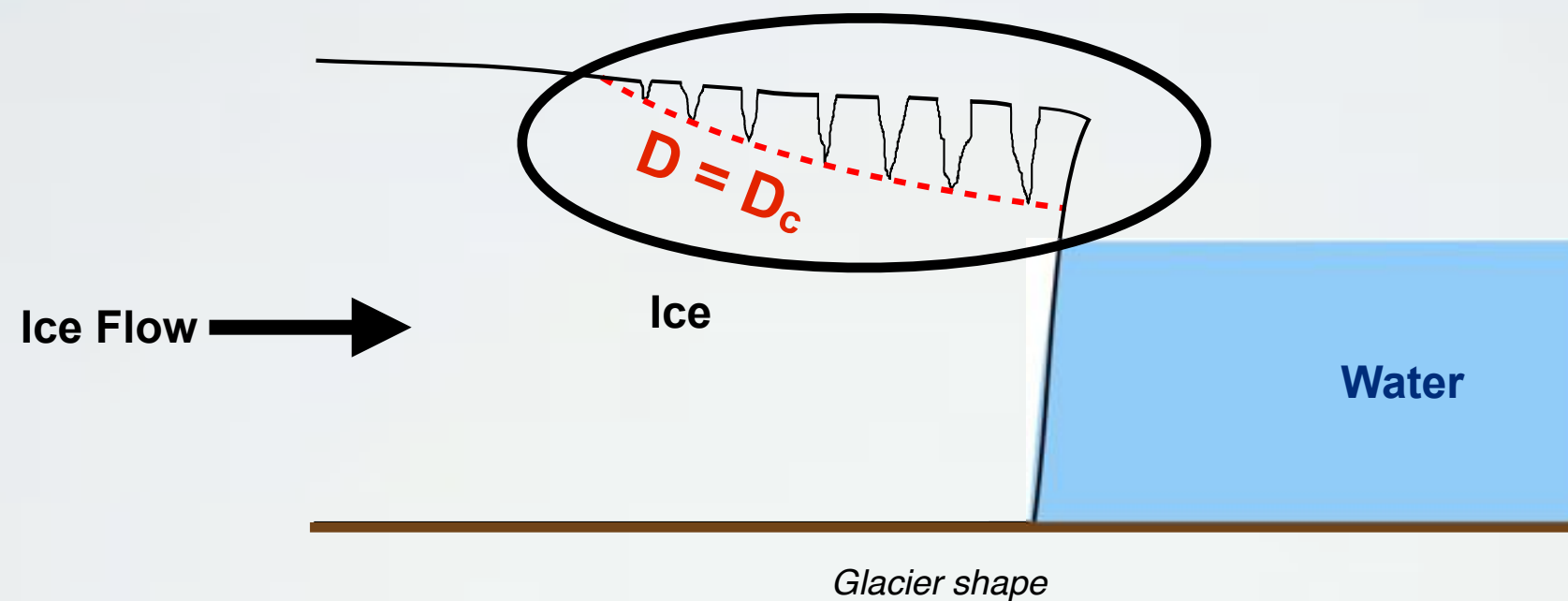
If $K_I > K_{Ia}$ at the bed, calving event
occurs along a vertical line.



Model Presentation - Linear Elastic Fracture Mechanics

CalvingSolver.f90

Get Dc
Contour



Model Presentation - Linear Elastic Fracture Mechanics

CalvingSolver.f90

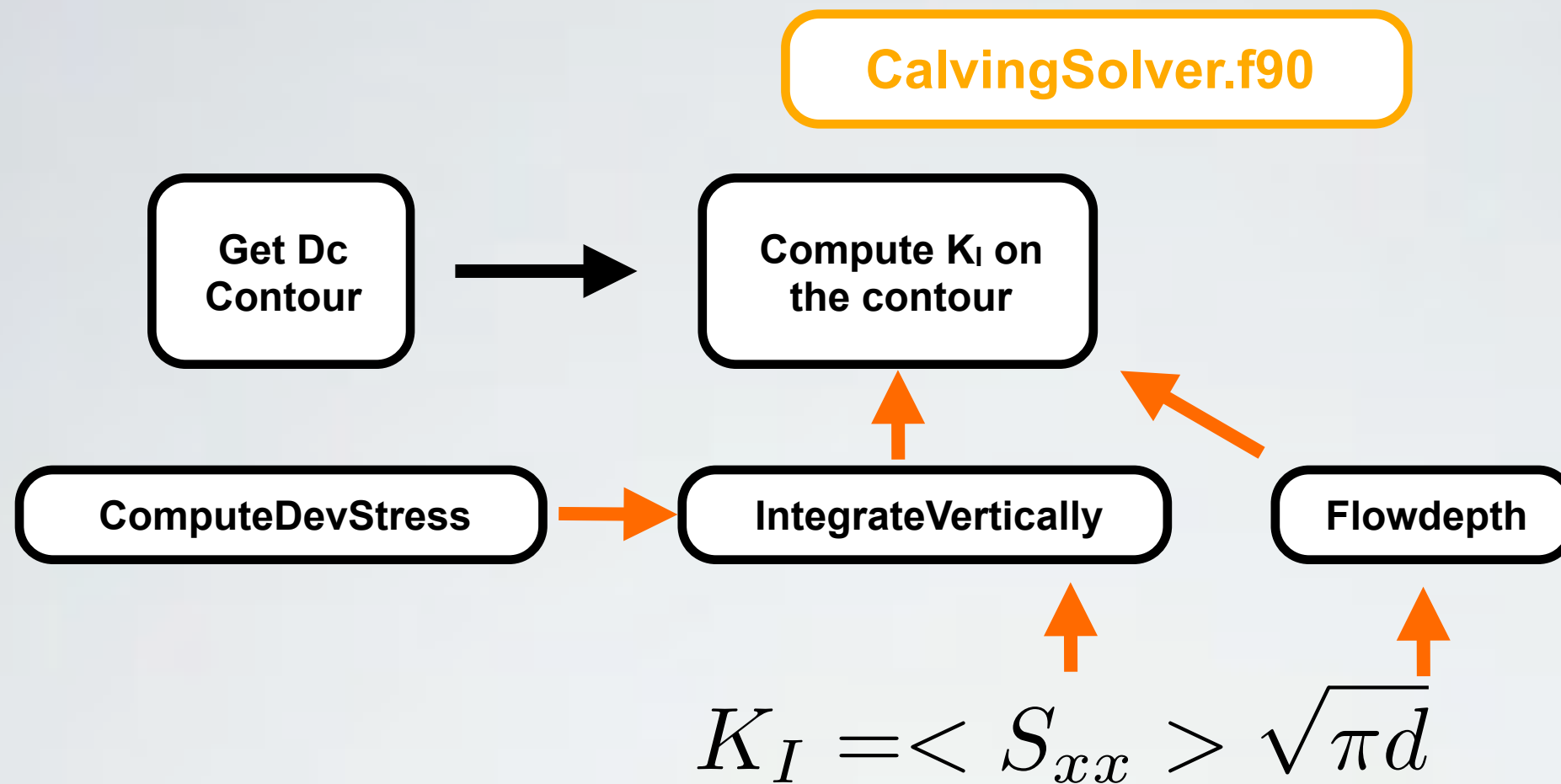
Get Dc
Contour



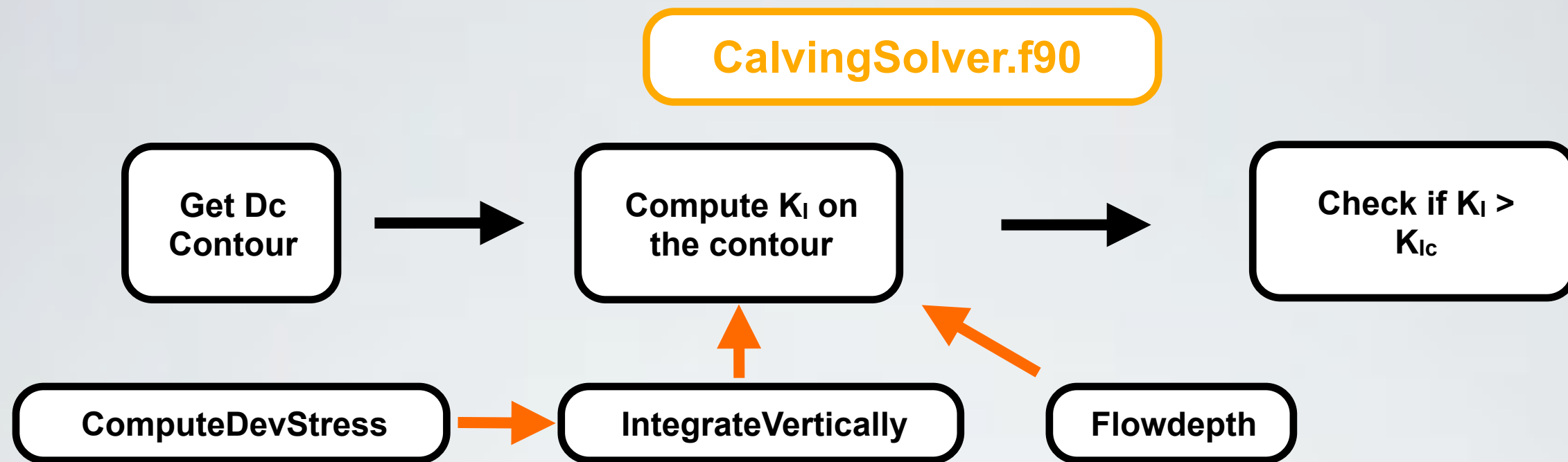
Compute K_I on
the contour

$$K_I = \langle S_{xx} \rangle \sqrt{\pi d}$$

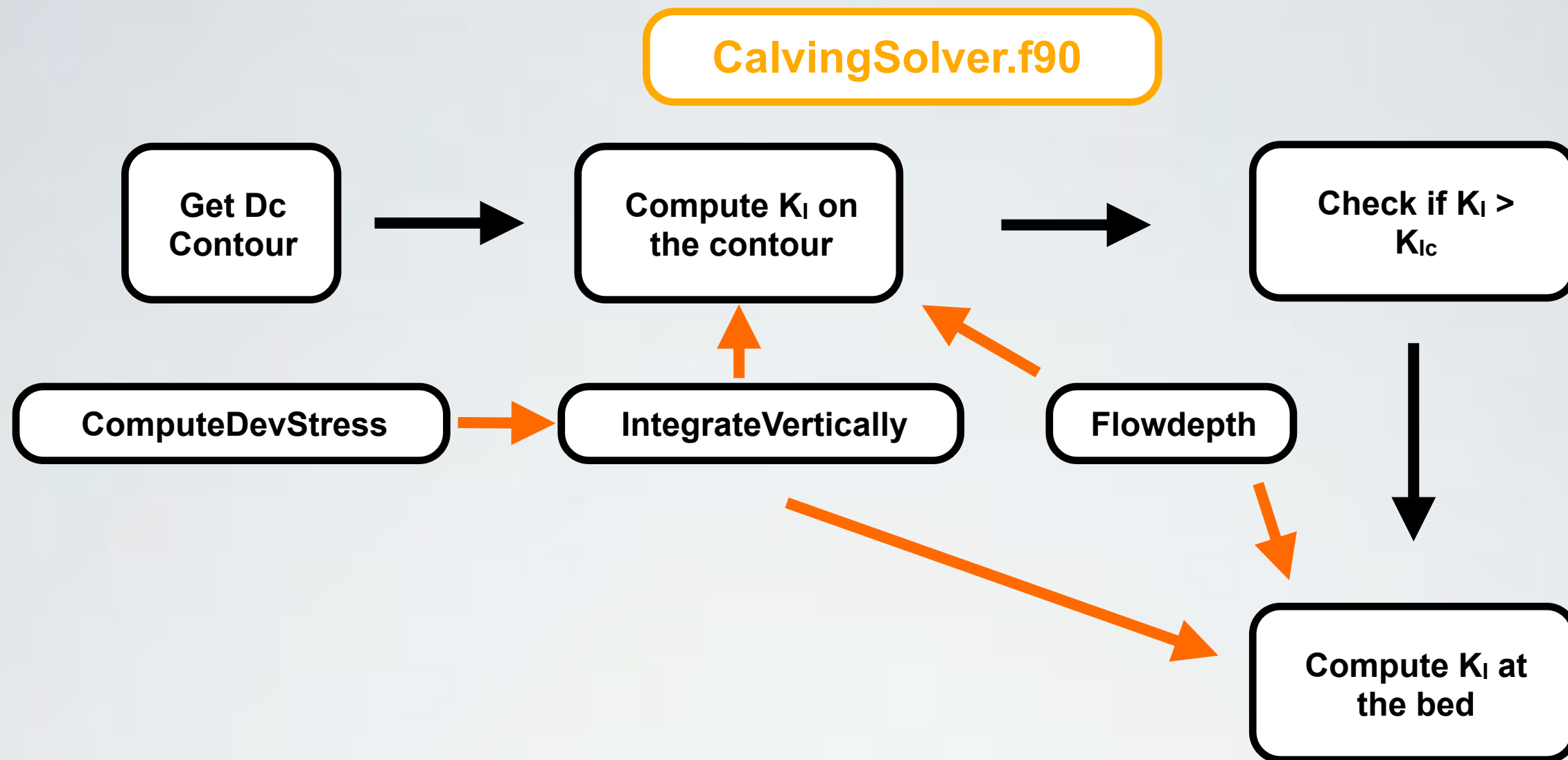
Model Presentation - Linear Elastic Fracture Mechanics



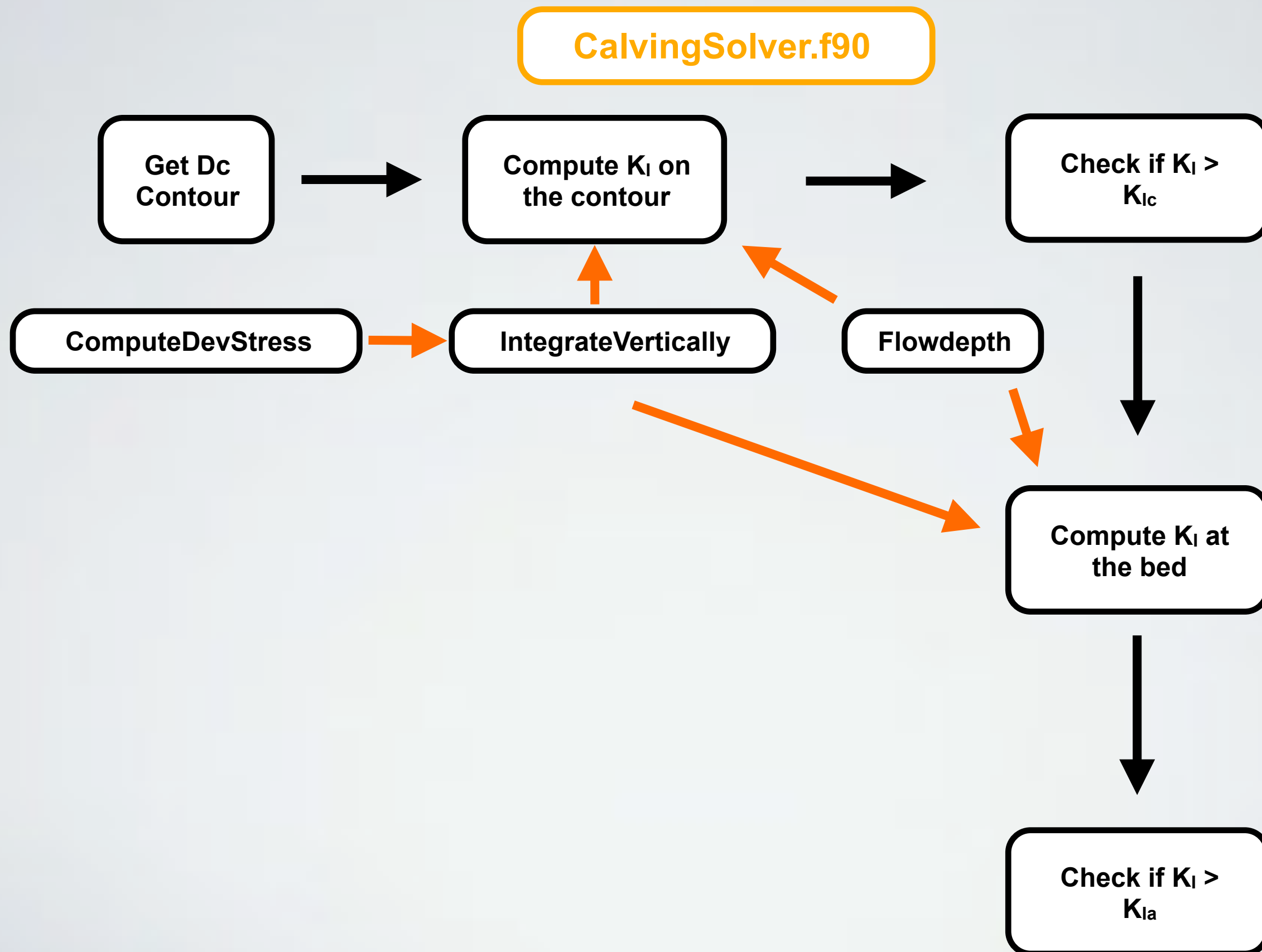
Model Presentation - Linear Elastic Fracture Mechanics



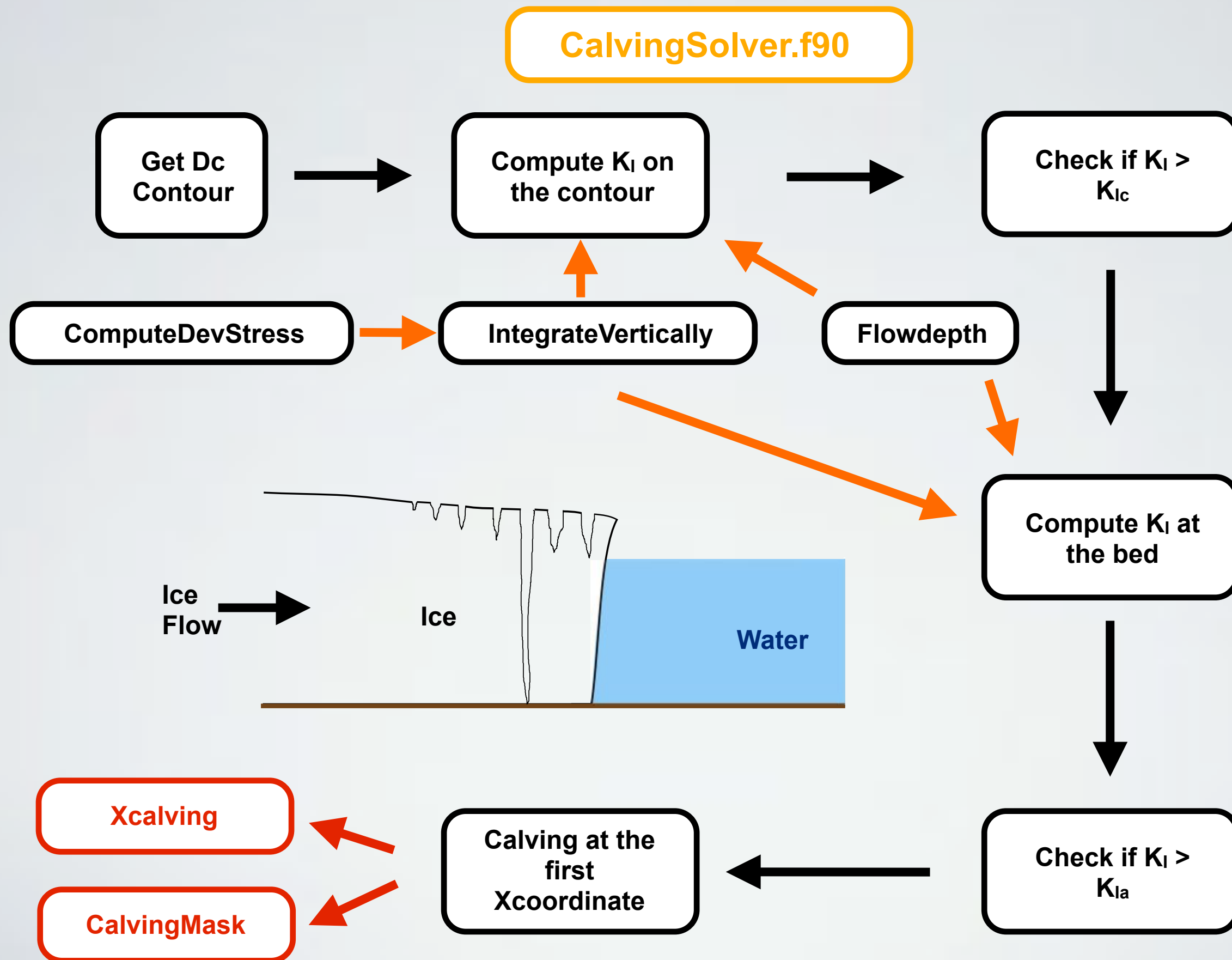
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Model Presentation - Linear Elastic Fracture Mechanics



Model Presentation - Linear Elastic Fracture Mechanics

CalvingSolver.f90

CalvingMask

Dc

K_{Ic}

α

with

$$K_{I_a} = \alpha \cdot K_{I_c}$$

```
Solver #
Class Solver = New
Equation = "CalvingSolver"
Variable = CalvingMask :CalvingMask
Variable DOFs = 1
Procedure = "../CalvingSolver" "CalvingSolver"

Active Coordinate = Integer 2

Critical Value = Real $CalvingCriterion (Real 8.0)
Critical Toughness = Real 0.150 1000
Crack Arrest Parameter = Real 0.5 1 1000 100000

Exported Variable 1 = Xcalving
Exported Variable 1 DOFS = 1
End
```

Xcalving

Model Presentation - Linear Elastic Fracture Mechanics

Initialization

```
Initial Condition 2
! sets the initial position of the free surface variable
Xf = Equals Coordinate 1
! reference to this initial condition
ReferenceXf = Equals Coordinate 1
Xcalving = Equals Coordinate 1
CalvingMask = Real -1.0
End
```

How to prescribe terminus retreat?

```
! Calving front (x=L) This is the free surface here
Boundary Condition 4
Target Boundaries = 2
Body Id = 2

! documenter si besoin d'un front mobile
Xf = Equals Xcalving
Xf Condition = Equals CalvingMask

Mesh Update 1 = Variable Xf, ReferenceXf
Real MATC "tx(0) - tx(1)"

Flux integrate = Logical True
```

Conclusion

Two distincts aspects :

- Damage Model -> USF_Damage.f90
- Calving Criterion -> CalvingSolver.f90

Prospectives / Limitations :

Damage Model :

- Extent the damage model for 3D/ Partitionned cases
- Improve the complexity of damage criterion
- Application on real cases

Calving Solver (not the priority):

- 3D developpement

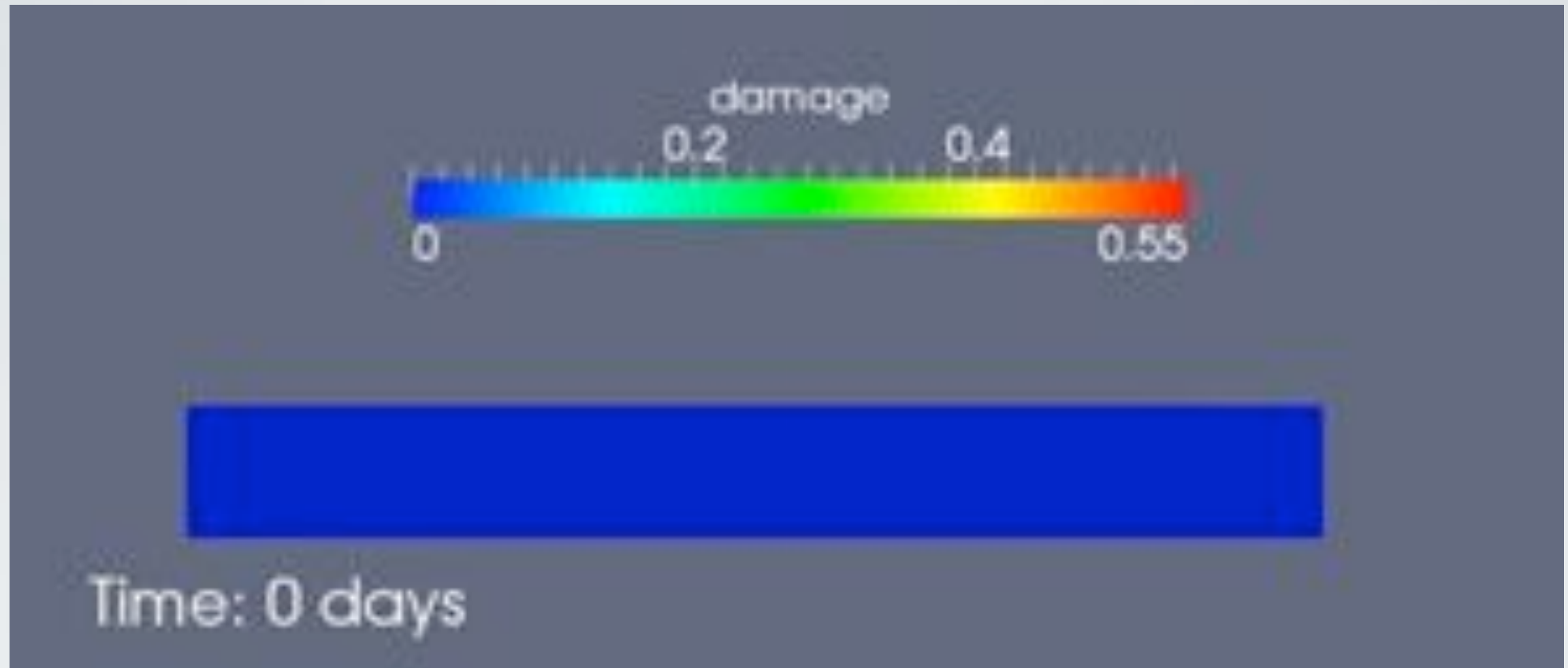


Work in progress !

Some results

With a sinusoidal frontal melt rate...

Some results



With a sinusoidal frontal melt rate...

Some results



With a sinusoidal frontal melt rate...

Thank you !

References

Van der Veen, C.J. « Fracture mechanics approach to penetration of bottom crevasses on glaciers ». Cold Regions Science and Technology 27, n° 3 (june 1998): 213–223. doi:10.1016/S0165-232X(98)00006-8.

Van der Veen, C.J. « Fracture mechanics approach to penetration of surface crevasses on glaciers ». Cold Regions Science and Technology 27, n° 1 (february 1998): 31–47. doi:10.1016/S0165-232X(97)00022-0.

Weiss, Jérôme. « Subcritical crack propagation as a mechanism of crevasse formation and iceberg calving ». Journal of Glaciology 50, n° 168 (2004): 109–115. doi:10.3189/172756504781830240.