



Simulating Antarctic subglacial hydrology processes beneath Pine Island Glacier, using GlaDS in Elmer/Ice

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Ice dynamics, basal hydrology, Antarctica, GlaDS, Elmer/ice, PIG

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Why important to study (simulate) subglacial hydrology system?

- Subglacial drainage system influences basal sliding
- Contribute to SLR and have an impact on SLR prediction
- Previous work on ice dynamics involves little hydrology feedback
- Difficult to directly observe subenvironment
- Couple hydrology model to ice dynamics may give more specific SLR

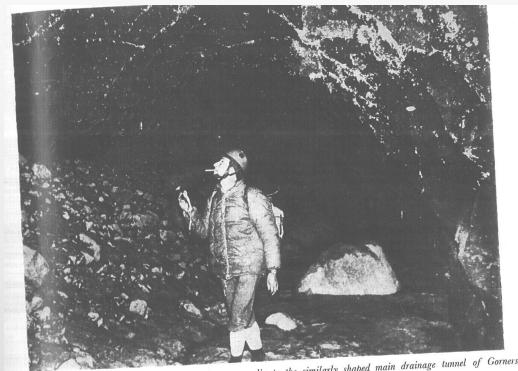


Fig. 11. Typical section of the duct leading from a moulin to the similarly shaped main drainage tunnel of Gornersee. (Photograph by Luc Vuadens, Groupe St. Exupéry).

Hydrology model developments

- Conduit model (Rothlisberger et al., 1972)
- Box model (Clarke et al., 1996)
- Flow-line model (Flowers et al., 2004)
- 2D network model (Schoof et al., 2012; Shugar et al., 2017)
- GlaDS, coupled distributed and continuous drainage model (Werder et al., 2013; Dow et al., 2016; Dow et al., 2020)

GlaDS model in Elmer/Ice

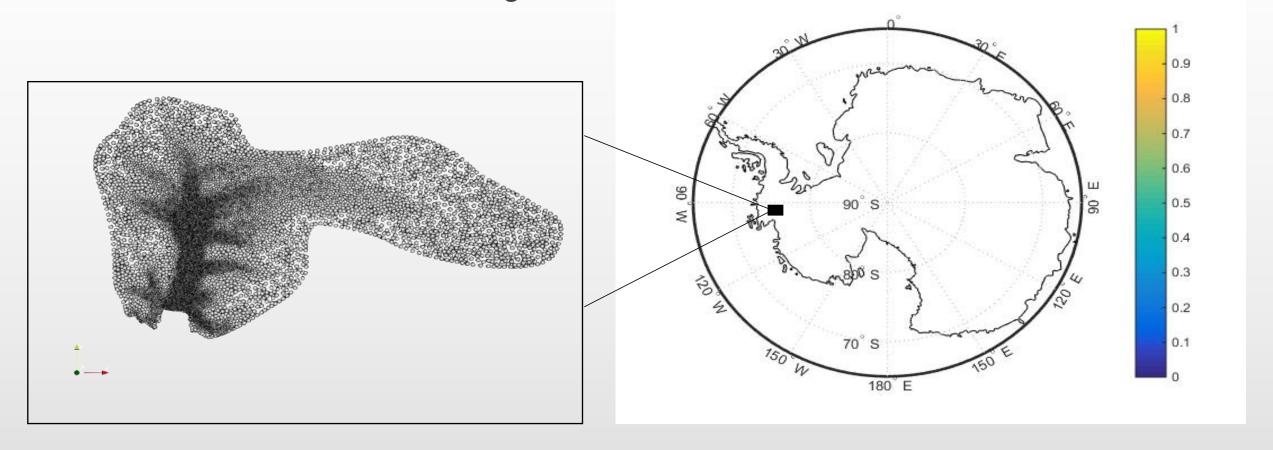
- Oliver Gagliardini, Mauro A. Werder., 2018
- de Fleurian et al., SHMIP project, 2017

My research work focus on applying GlaDS in Elmer/Ice to a marineterminating glacier, Pine Island Glacier, West Antarctica, to reveal realistic hydrology system and test centurial timescale evolution under climate senarios.

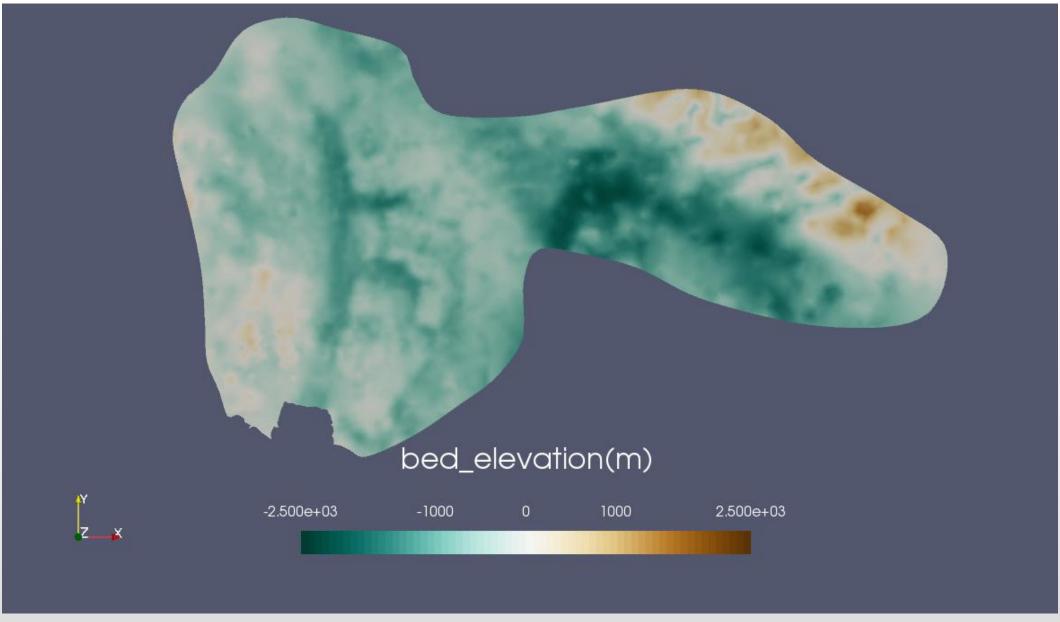
Reason of choosing Pine Island Glacier, West Antarcitca

One of the biggest mass loss and contribution to SLR.

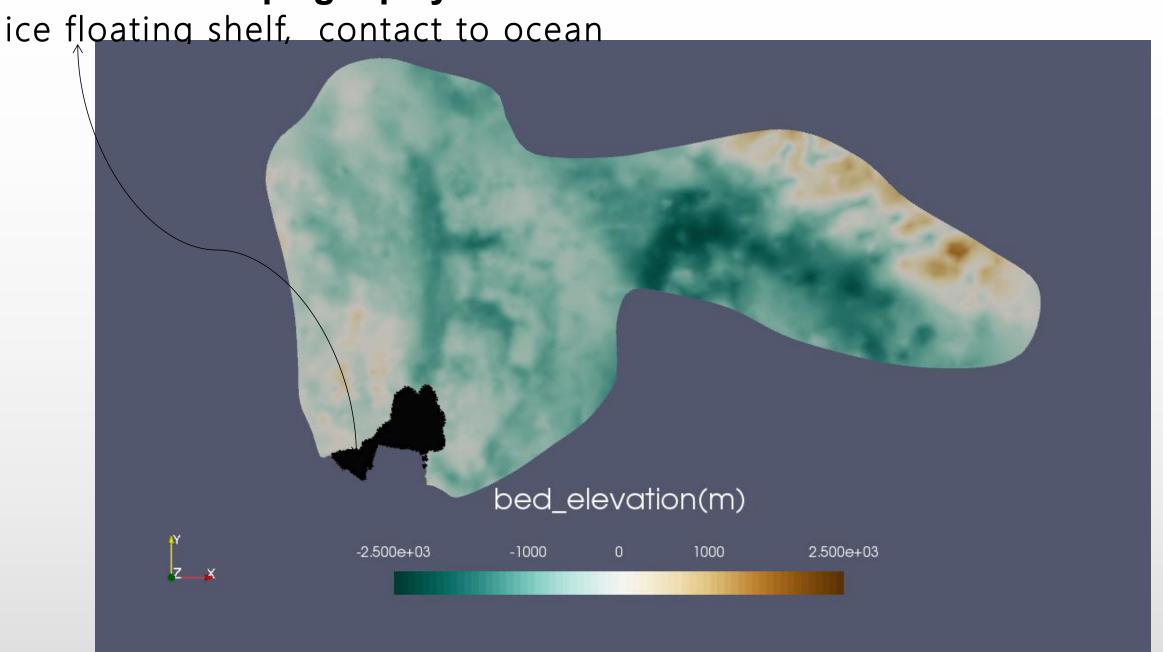
• One of the fatest retreated glacier, 4000 m s⁻¹



Domain & Topography trough in the center of PIG

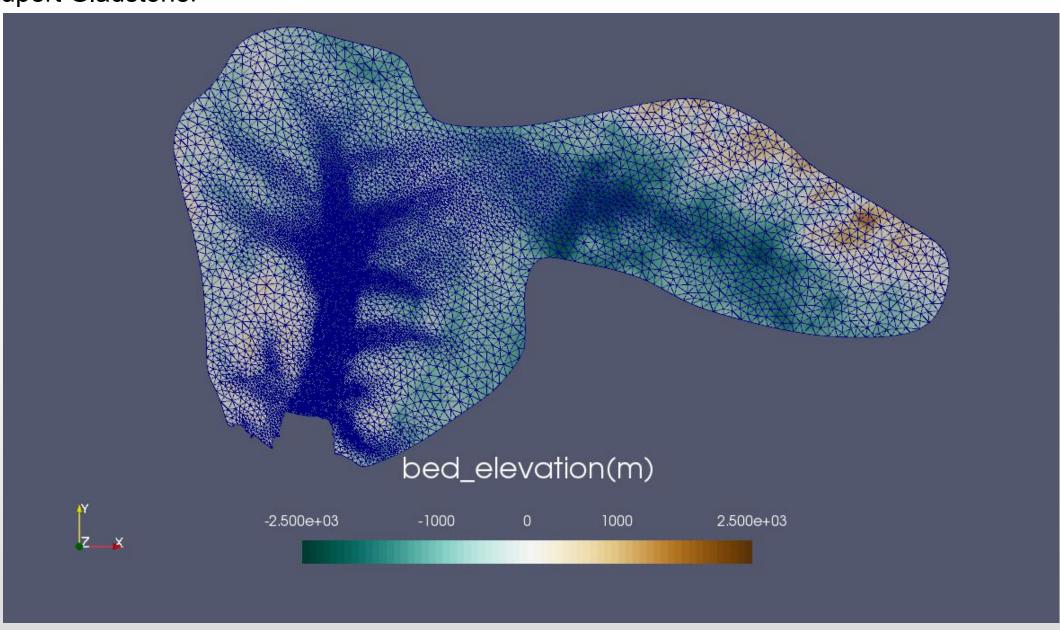


Domain & Topography



Unstructed triangle mesh; Different density

from Rupert Gladstone.



Bodys and Boundary Condition

- including 3 bodys, one shared body
- BC, set on lower surface, inland
- Direchelet BC: HP,N,Pw = 0
- Run 2000 days (over 4 years), output every 50 days
- waterinput1: Constant Water Input = 0.01m a⁻¹

Parameters

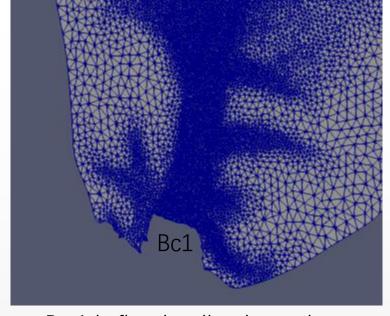
parameters and equations controls hydrology process

Table 1. Parameters and Values Used in Synthetic Model Runs^a

Description	Symbol	Value	Units
Acceleration due to gravity	g	9.81	m s ⁻²
Latent heat	L	3.34×10^{5}	$J kg^{-1}$
Ice density	ρ_i	910	$kg m^{-3}$
Water density	ρ_w	1000	$kg m^{-3}$
Pressure melt coefficient	c_t	7.5×10^{-8}	K Pa ⁻¹
Heat capacity of water	c_w	4.22×10^{3}	$J kg^{-1} K^{-1}$
First sheet flow exponent	α	5/4	
Second sheet flow exponent	β	3/2	
First channel flow exponent	α_c	5/4	
Second channel flow exponent	β_c	3/2	
Sheet conductivity ^b	k	0.01	$m^{7/4} kg^{-1/2}$
Channel conductivity ^c	k_c	0.1	$m^{3/2} kg^{-1/2}$
Glen's n	n	3	
Ice flow constant cavities	\tilde{A} \tilde{A} \tilde{A}_c	5×10^{-25}	$Pa^{-n} s^{-1}$
Ice flow constant channels	\tilde{A}_c	5×10^{-25}	$Pa^{-n} s^{-1}$
Basal sliding speed	u_b	10^{-6}	$m s^{-1}$
Sheet width below channeld	l_c	2	m
Cavity spacing	l_r	2	m
Bedrock bump height	h_r	0.1	m
Englacial void ratio	e_v	10^{-3}	
Moulin cross-sectional area	A_m	10	m^2
Bed elevation	B		m
Ice thickness	H		m
Sheet input	m		$m s^{-1}$
Moulin input	Q_s		$m^3 s^{-1}$

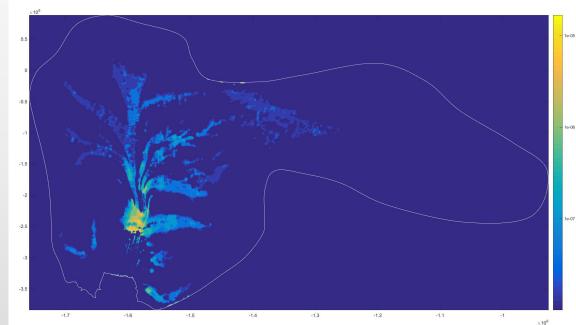
Table 2. Variables and Units^a

Description	Variable	Units
Hydraulic potential	φ	
Channel discharge	Q S	$m^3 s^-$
Channel cross-sectional area	S	m ²
Sheet discharge	q	$m^2 s^-$
Sheet thickness	h	m
Time coordinate	t	S
Along edge coordinate	S	m
Normal vector	n	m
Test function	θ	Pa
Englacial storage	h_e	m
Hydraulic potential of bed	ϕ_m	Pa
Overburden hydraulic potential	ϕ_0	Pa
Effective pressure	N	Pa
Cavity opening rate	w	$m s^{-1}$
Cavity closure rate	ν	$m s^{-1}$
Channel dissipation	П	$W m^-$
Channel press-melt	Ξ	$W m^-$
Channel closure rate	v_c	$m^2 s^{-1}$
Sheet flow beneath channel	q_c	$m^2 s^{-1}$
Water volume in moulin	V_m	m^3



Bc 1 is floating line boundary.

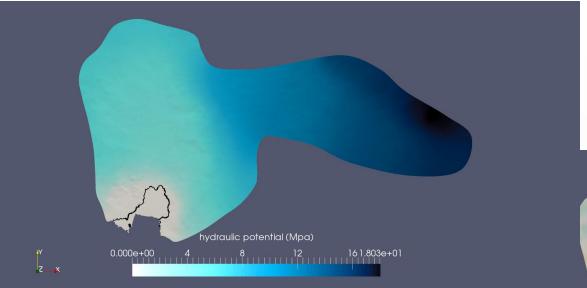
Water Input 2 from inversion model



outputs: hydraulic potential, ice discharge, effective pressure

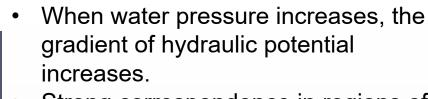
Results 800days

Hydraulic potential

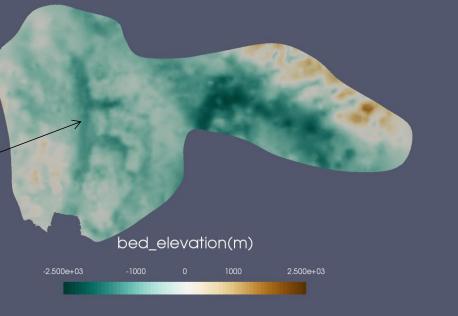


water pressure (Mpa)

Water Pressure

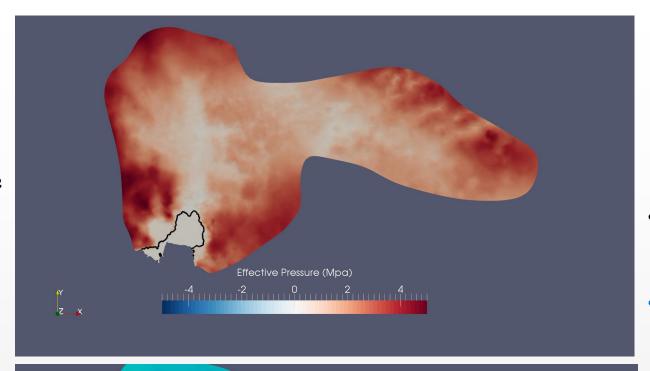


Strong correspondence in regions of faster sliding velocity with high water pressure. (along the troughs)



Results 800days

Effective Pressure

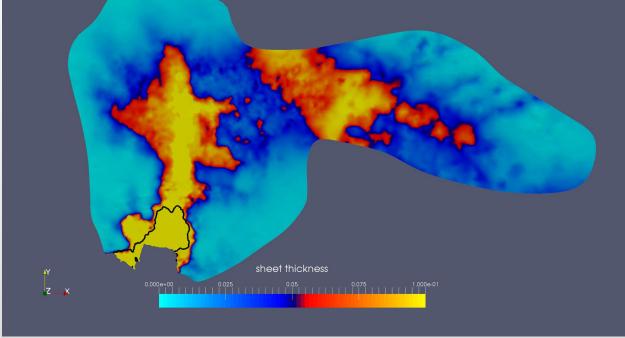


with presnece of sheet thickness.

Agreement of high water pressure

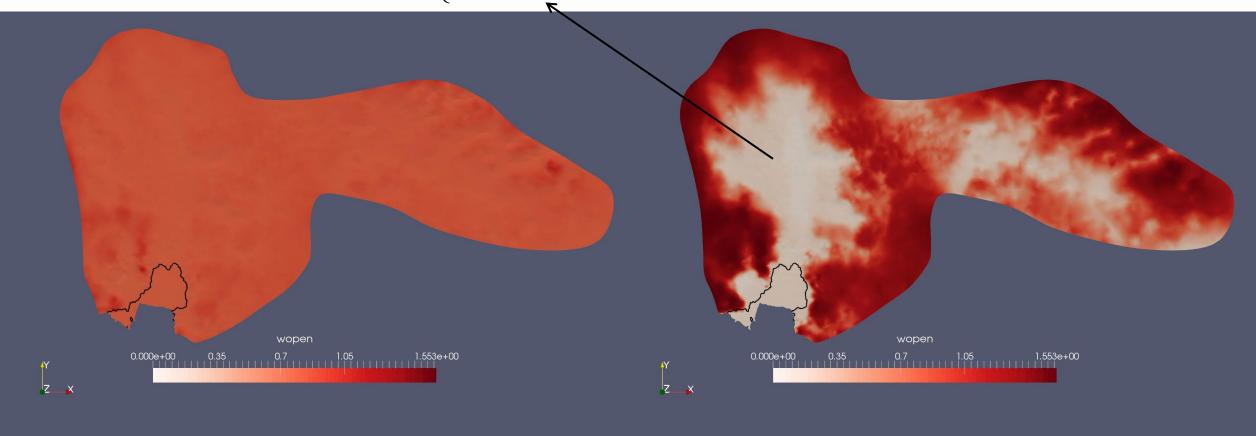
 Water pressure is basicly the same with ice overburden pressure.

Sheet thickness



Results cavity opening rate

$$\mathbf{w} \ (h) = \begin{cases} \frac{u_b \left(h_r - h\right)}{l_r}, \ h < h_r & h_r = 0.1 \text{(m)} \quad l_r = 2 \text{(m)} \\ 0, \ otherwise & \text{sheet thickness is bigger than height of bed bump.} \end{cases}$$



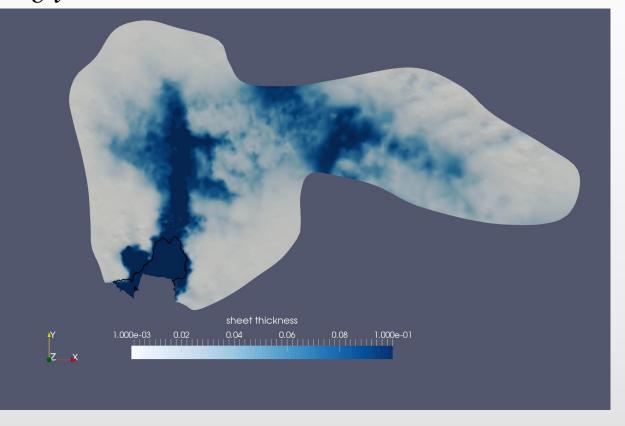
water input1

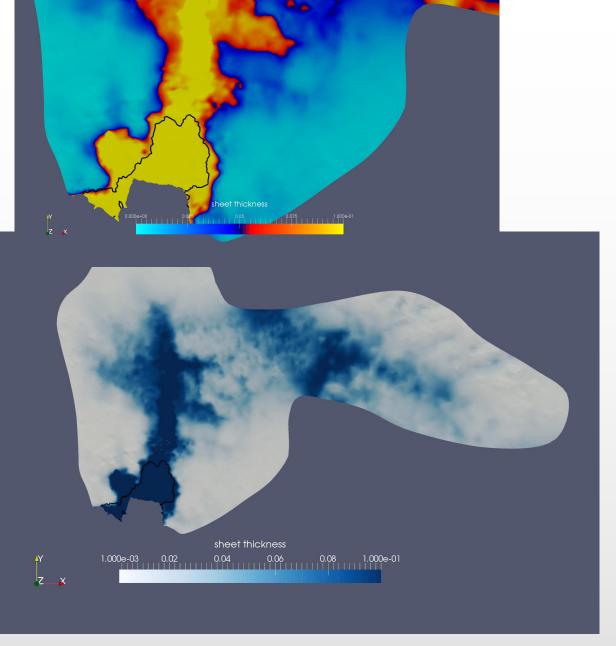
Results

Sheet thickness

h [0.001,0.1] m

$$\frac{\partial h}{\partial t} = w - v$$





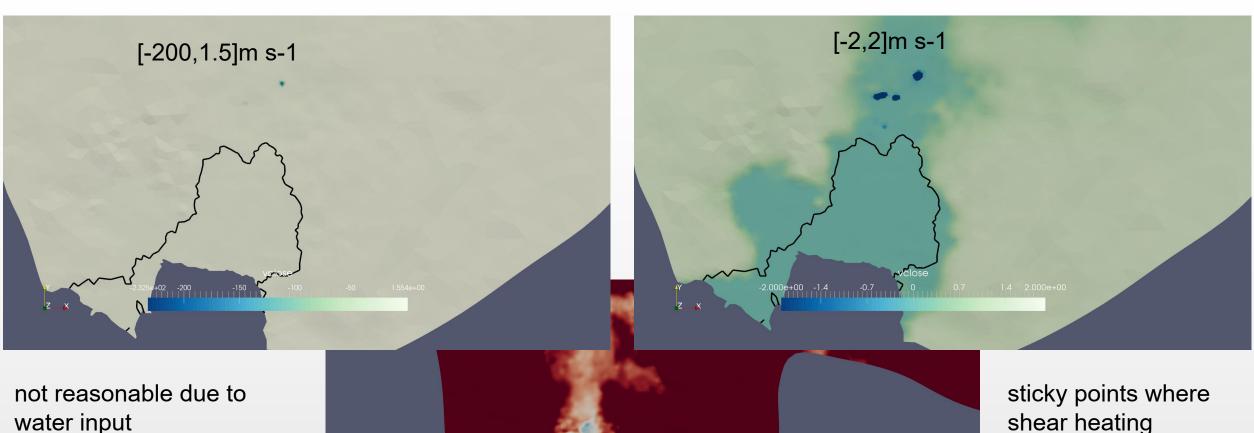
800days

850days

$$\mathbf{v}(h,N) = \mathbf{A}h \big| N \big|^{n-1} N$$

Y Z X

800days



Effective Pressure (Mpa) -0.7 -0.35 0 0.35 0.7

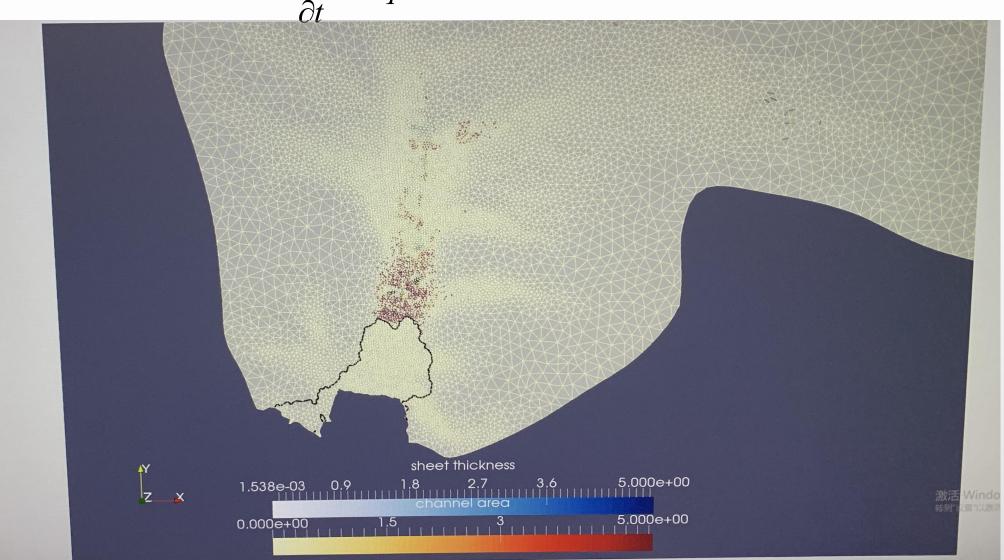
water input

shear heating accumulates.

Results

Sheet thickness channel evoving

h [0.001,0.1] m S [0,5] m² $\frac{\partial h}{\partial t} = w - v$ $\frac{\partial h}{\partial t} + \nabla q = m$



Results

800days

qx

sheet discharge Y

$$q = -\kappa h^{\alpha} |\nabla \phi|^{\beta - 2} \nabla \phi$$

$$\frac{\partial h}{\partial t} + \nabla q = m$$

High water pressure consistent with more sheet discharge.

qy

Outlook

- Need further realistic water input to drive Glads from inversion model
- Need more results analysis and sensitivity tests
- Couple model with ice dynamics, give more realistic and detailed results.
- Couple to ocean model to simulate ocean circulation.



Thank you!

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