



Elmer/Ice advanced workshop 2017



Grenoble, France



CSC – Finnish research, education, culture and public administration ICT knowledge center

How to write your own solver

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Outline

- We will discuss how to implement a simple Darcy flow problem
- We will discuss the derivation of the weak formulation from the PDE
- We will discuss the implementation of different (incl. natural) boundary conditions
- We will show how to modify the existing blueprint for advection-diffusion equations, Elmer's ModelPDE
- We will show how to compile the solver and how to include it in the SIF

Darcy flow

- Describes saturated flow in porous media
- Based on continuity of the groundwater flux, \mathbf{J}_{gw} :

$$\nabla \cdot \mathbf{J}_{gw} = S_{gw}$$

Where S_{gw} is the volumetric source of water

- The flux usually is given by

$$\mathbf{J}_{gw} = \mathbf{K}_{gw} \cdot (\rho_w \mathbf{g} - \nabla p)$$

Where \mathbf{K}_{gw} is the (usually tensor-valued) hydraulic conductivity

NB: often the hydraulic head, including hydrostatic contribution is used instead – not so here

Weak formulation

- Applying weak formulation, i.e., integrating with test-function φ over whole domain Ω

$$\int_{\Omega} \nabla \cdot \mathbf{J}_{gw} \varphi dV = \int_{\Omega} S_{gw} \varphi dV$$

- Partial integration of l.h.s:

$$\int_{\Omega} \nabla \cdot (\mathbf{J}_{gw} \varphi) dV - \int_{\Omega} \mathbf{J}_{gw} \cdot \nabla \varphi dV = \int_{\Omega} S_{gw} \varphi dV$$

- Applying Green's¹⁾ theorem:

$$\oint_{\partial\Omega} \mathbf{J}_{gw} \cdot \mathbf{n} \varphi dV - \int_{\Omega} \mathbf{J}_{gw} \cdot \nabla \varphi dV = \int_{\Omega} S_{gw} \varphi dV$$

¹⁾Gauss, for the German speakers

Weak formulation

- Inserting and rearranging for the unknown, the pressure:

$$\int_{\Omega} (\mathbf{K}_{gw} \cdot \nabla p) \cdot \nabla \varphi \, dV = \int_{\Omega} (\mathbf{K}_{gw} \cdot \mathbf{g} \rho_w) \cdot \nabla \varphi \, dV + \int_{\Omega} S_{gw} \varphi \, dV - \int_{\partial\Omega} \mathbf{J}_{gw} \cdot \mathbf{n} \varphi \, dV$$

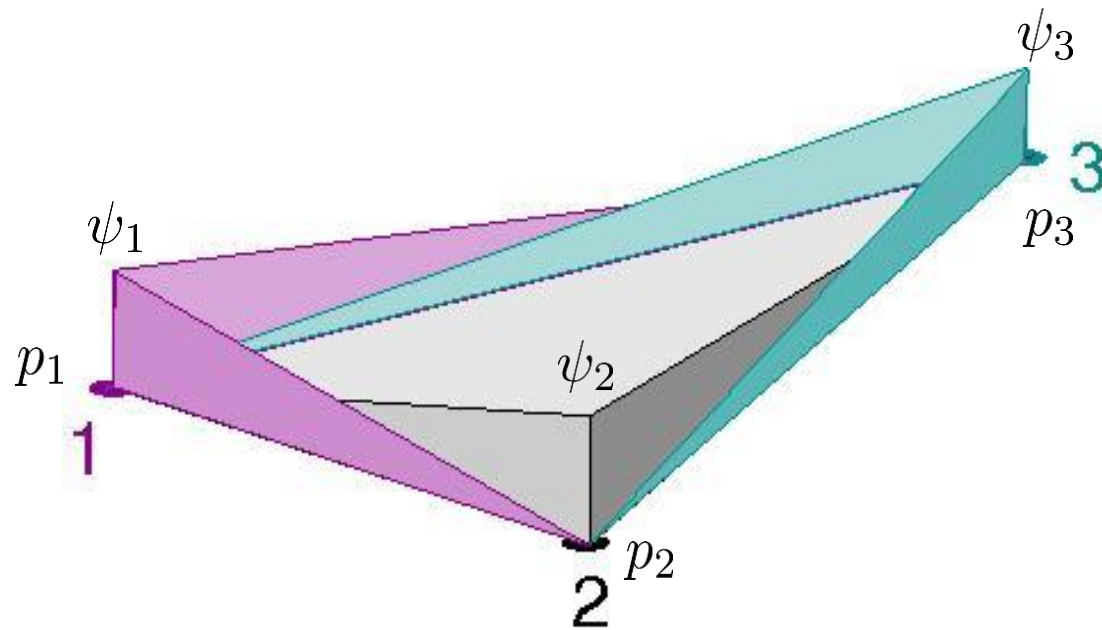
Left hand side

Body force
(a.k.a. right hand side)

Natural boundary
condition

Discrete matrix formulation

- Expressing variable (=pressure) inside element as the sum of the nodal values multiplied by weighting functions (= *standard Galerkin method*)



$$p(\mathbf{x}) = \sum_{i=1}^3 p_i \psi_i$$

Discrete matrix formulation

- Taking weighting and test-functions to be the same:

$$p_i \int_{\Omega} (\mathbf{K}_{gw} \cdot \nabla \varphi_i) \cdot \nabla \varphi_j dV = \int_{\Omega} (\mathbf{K}_{gw} \cdot \mathbf{g} \rho_w) \cdot \nabla \varphi_j dV + \int_{\Omega} S_{gw} \varphi_j dV - \int_{\partial\Omega} \mathbf{J}_{gw} \cdot \mathbf{n} \varphi_j dV$$

$$p_i M_{ij}$$

=

$$F_j$$

$$- \int_{\partial\Omega} \mathbf{J}_{gw} \cdot \mathbf{n} \varphi_j dV$$

Solution vector System matrix

Body force

Natural boundary condition

Some simplifications

- Ignoring tensor-valued hydrological conductivity tensor (scalar diffusivity)

$$\mathbf{K}_{gw} = \mathbf{1} (k_{gw} / \mu_{H_2O}) = \mathbf{1} K_{gw}$$

◦ Where k_{gw} is the hydraulic conductivity

$$p_i \int_{\Omega} K_{gw} \nabla \varphi_i \cdot \nabla \varphi_j dV = \int_{\Omega} K_{gw} \rho_w \mathbf{g} \cdot \nabla \varphi_j dV + \int_{\Omega} S_{gw} \varphi_j dV - \oint_{\partial\Omega} \mathbf{J}_{gw} \cdot \mathbf{n} \varphi_j dV$$

`Weight * K * MATMUL(dBasisdx, TRANSPOSE(dBasisdx))`

`Weight * K * rho * SUM(Gravity(1:DIM), dBasisdx))`

Output of Variable

- We want to simply have the identity as variable (= solution):

$$\mathbf{J}_{gw} = \mathbf{K}_{gw} \cdot (\rho_w \mathbf{g} - \nabla p)$$

- We do the identity component-wise:

$$J_i = K_{gw} (\rho_w g_i - \nabla_i p)$$

- Or in weak formulation:

$$\int_{\Omega} J_i dV = \int_{\Omega} K_{gw} (\rho_w g_i - \nabla_i p)$$

Discrete matrix formulation

- Taking weighting and test-functions to be the same:

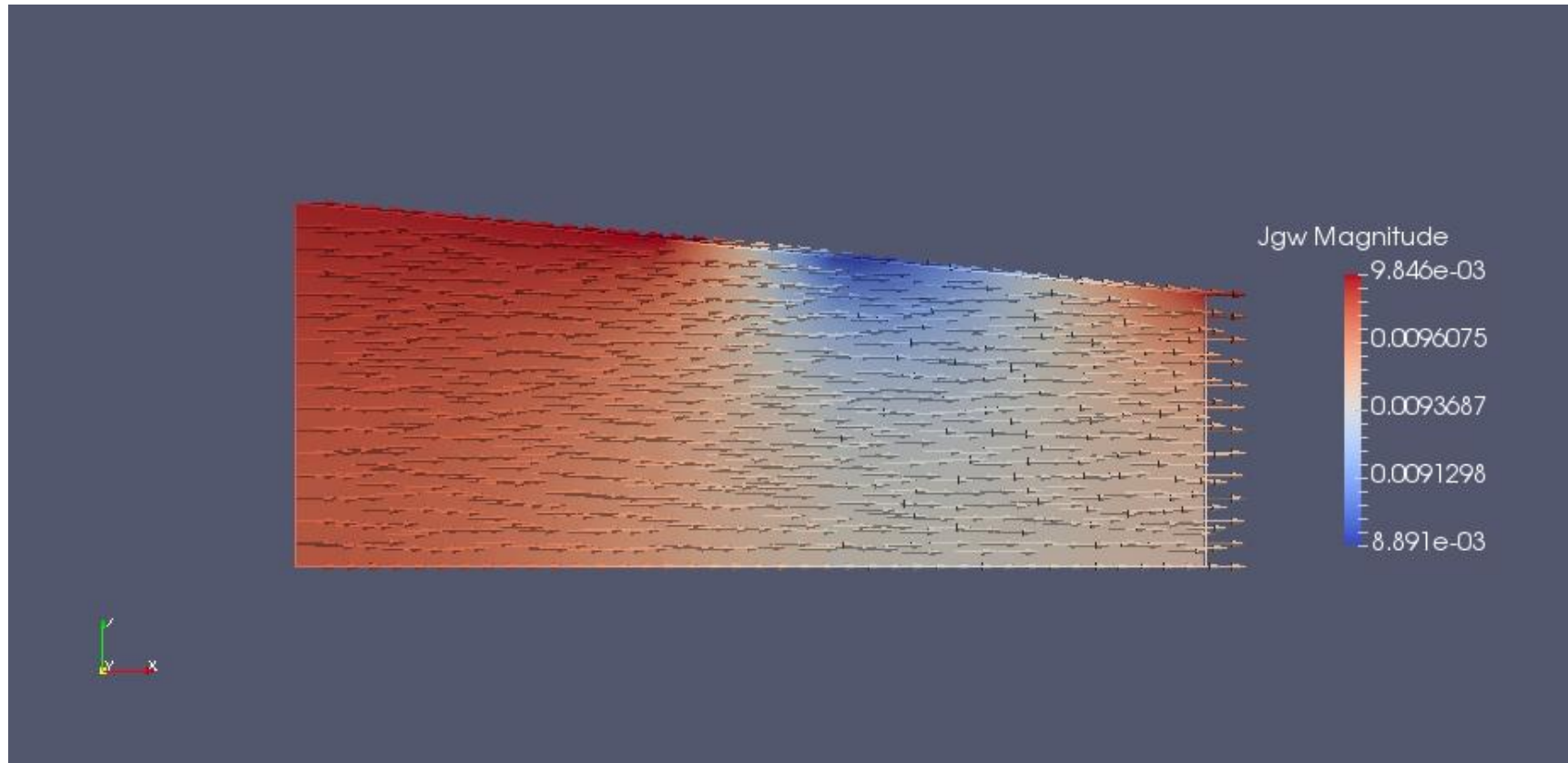
$$J_{\alpha,i} \int_{\Omega} \varphi_i \varphi_j dV = \int_{\Omega} K_{gw} (g_{\alpha} - \nabla_{\alpha} p) \varphi_j dV$$

$$J_i M_{ij} = F_j$$

Solution vector System matrix

Body force

Darcy flux



Heat transfer

- With the computed flux, we want to advect/diffuse a temperature field

$$\bar{c}_p \frac{\partial T}{\partial t} + \rho_w c_w \mathbf{J}_{gw} \cdot \nabla T = \nabla \cdot (\bar{\kappa} \nabla T)$$

Time
derivative
coefficient

convection
coefficient

convection
velocity

diffusion
coefficient

Material 1

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Convection Velocity 1 = Equals Flux1
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Convection Velocity 2 = Equals Flux2
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Convection Velocity 3 = Equals Flux3
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time derivative coefficient = Real $porosity * waterheatcap * waterdens + (1.0 - porosity)*soilheatcap*soildens
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diffusion coefficient = Real $porosity * waterheatcon + (1.0 - porosity)*soilheatcon
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convection coefficient = Real $waterheatcap * waterdens
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reaction coefficient = Real 0.0
```

Heat transfer

